July 14, 2017 Revised August 8, 2017

City of Mission Planning & Zoning Department 6090 Woodson Mission, KS 66202

**RE:** Mission Trails FDP – Final Stormwater Summary

Dear City:

This letter summarizes final stormwater calculations to support the proposed Mission Trails mixed use project at 6201 Johnson Drive. The project includes retail, multi-story residential, and a parking garage.

An existing one story building and surface parking lot is located on the 2.82 acre site. Most of the site discharges to the southeast to storm infrastructure along Beverly Avenue. The remainder drains to curb inlets on the south side of Johnson Drive. Approximately 0.52 acres of offsite drainage area from the Salvation Army site to the west drains onto the site. Much of the site is covered with impervious building, parking, and walking surfaces, resulting in 2.30 acres or 81.6% of the total site area. The underlying soils are Sharpsburg-Urban land complex, 4 to 8 percent slopes, with a hydrologic soil group rating of C. The hydrologic soil group rating has been downgraded to D soils, to account for significant previous development on the site. See attached Exhibit A for a delineation of existing pervious area and drainage boundaries. The site lies within flood zone X (areas outside the limits of the 0.2% annual chance floodplain); see attached Exhibit B for a FEMA flood insurance rate map.

The proposed condition removes the existing building and parking lot. The proposed multi-story building with courtyard and parking garage will cover 1.98 acres of the site, with open space, sidewalks, and surface parking accounting for the balance of 0.84 acres. The proposed impervious area is 2.33 acres or 82.6% of the total site area. This is a modest increase in impervious area over existing conditions of 1,152 square feet. As the incremental increase in impervious area is less than 5,000 square feet for this redevelopment project, APWA 5600 allows an exemption from stormwater detention requirements. This exemption also extends to the inclusion of MARC Best Management Practices (BMP's) for Stormwater Quality on the project. Therefore no stormwater detention or BMP's are proposed for this project. See attached Exhibit C for a delineation of proposed pervious area and drainage boundaries.

The table below summarizes the peak site discharge rate for existing and proposed conditions, for a SCS Type II 24-hour rainfall. There is not a significant enough change in impervious area to change the CN between existing and proposed conditions. The proposed impervious area calculations do account for 3,820 square feet of pervious area within the courtyard area.

Condition	Area	CN	Tc (min)	Peak Discharge		
	(ac)			50% storm (cfs)	10% storm (cfs)	1% storm (cfs)
Existing	2.82	95 (94.68)	5	13.15	19.87	30.03
Proposed	2.82	95 (94.87)	5	13.15	19.87	30.03

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All of the flow from the proposed building, parking garage, and offsite tributary runoff from the Salvation Army site will be captured in enclosed storm sewer systems and piped to the existing storm sewer infrastructure on Beverly Avenue. A swale is provided along the south side of the property to convey runoff from the 0.85 acre drainage area west and south of the building, should the enclosed storm sewer become clogged. The area north of the building will surface drain to Johnson Drive, as it does in the existing condition. See attached Hydraflow Hydrographs Report for summary of peak discharge rate calculations, and attached Bentley Flowmaster Report for a summary of the south swale capacity for the 1% storm event and full flow swale capacity. The cross section for the swale calculation is conservatively located near the southwest corner of the building where the running swale slope is the lowest. The swale capacity increases further downstream to the east where the running slope increases and the sideslopes become flatter.

An emergency overflow pipe is proposed from the internal courtyard area to the swale on the south side of the property. This backup measure provides redundancy in the event the internal courtyard storm conveyance system or downstream receiving system becomes clogged, to provide an additional protection measure for residences and businesses on the first floor of the building.

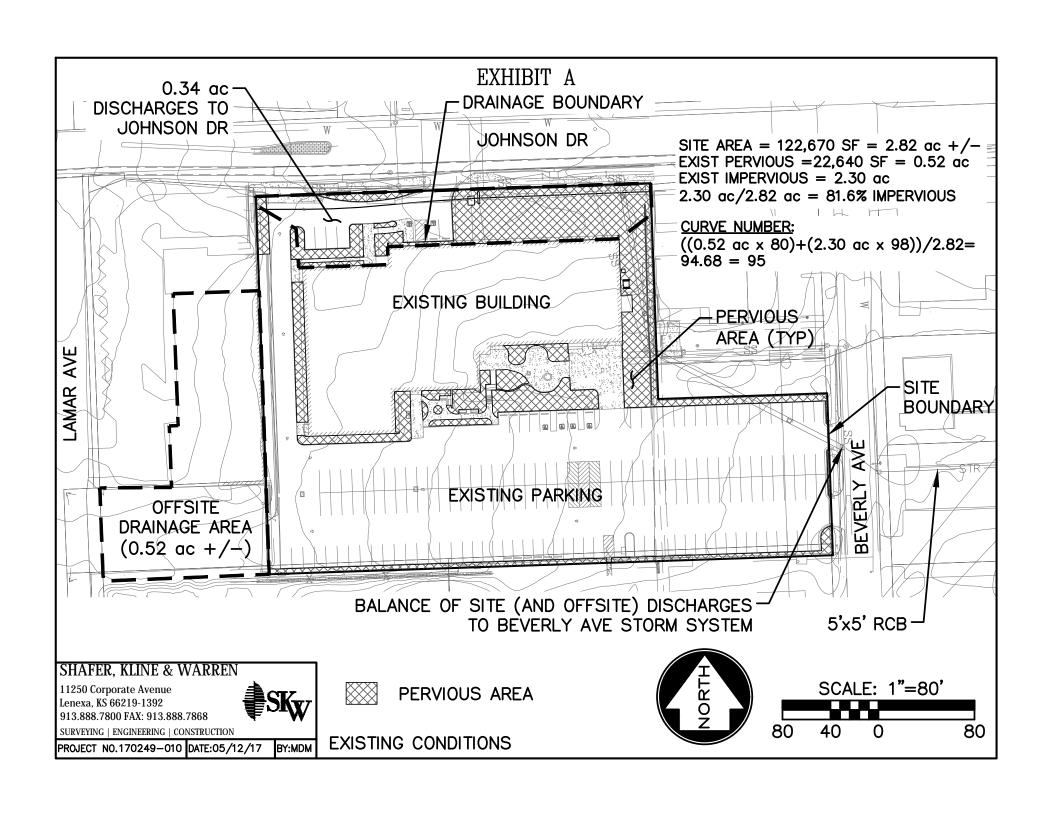
The site discharges to an existing 5'x5' box culvert at Beverly Avenue. The size is derived from AIMS data and the outfall pipe measurement at Rock Creek, as the box itself is not accessible from the Beverly Avenue curb inlets. The Johnson Drive Improvement project added a 7'x6' box culvert along Johnson Drive, and redirected approximately 75 acres of watershed north of Johnson Drive that used to discharge to the Mission Trails site outfall. Therefore the 5'x5' box culvert currently only receives approximately 3.9 acres of tributary area (project site + bar) at the site outfall location, with a peak 1% storm flow rate of 41.5 cfs. The box culvert has a full flow manning's capacity of 487.33 cfs across Beverly, therefore the downstream storm system in the vicinity of this site has sufficient capacity. See attached Bentley Flowmaster Report for a summary of the box culvert capacity calculation.

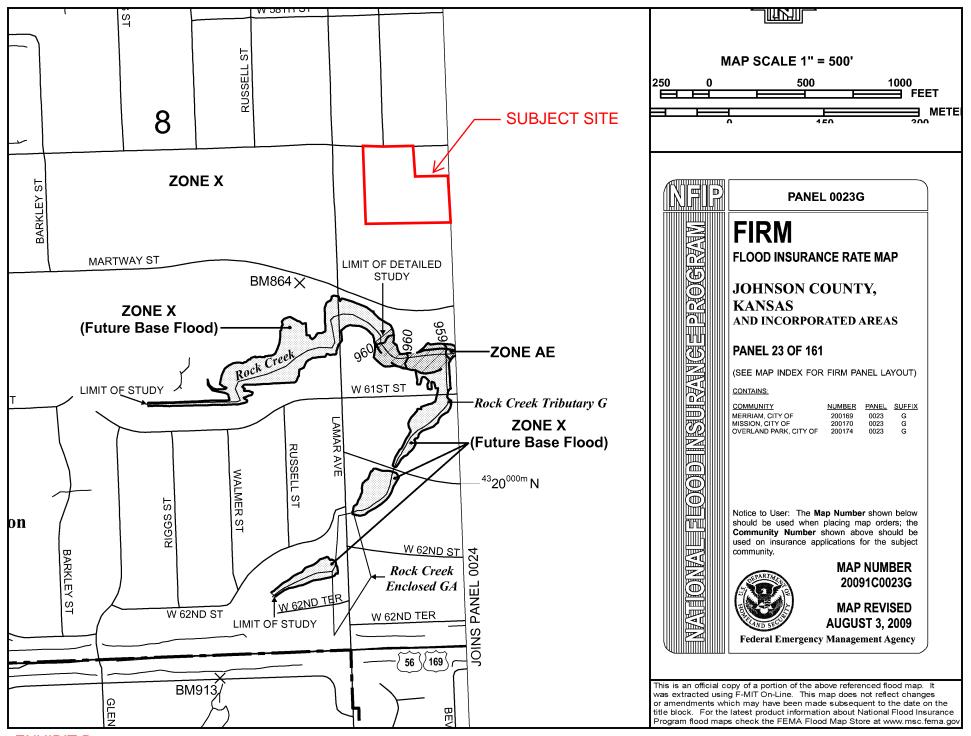
Please contact Matt Kist, P.E., or Dan McGhee, P.E., should you have any questions regarding this letter.

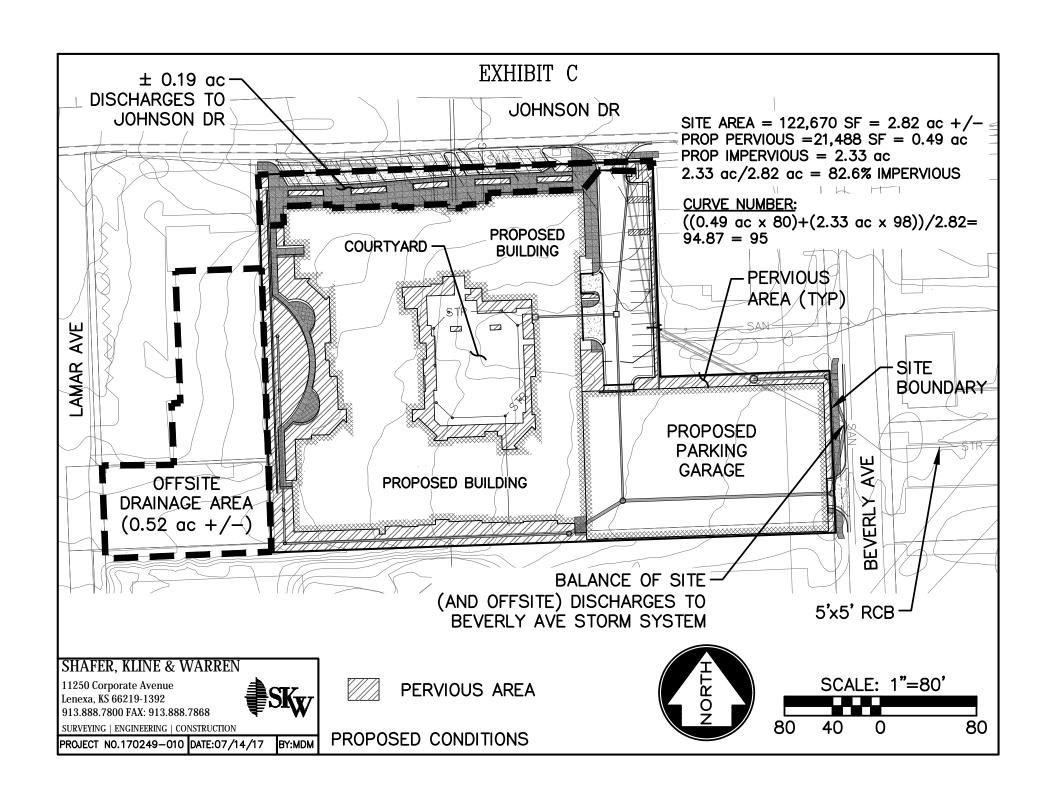
SHAFER, KLINE & WARREN, INC.

Enclosure(s)









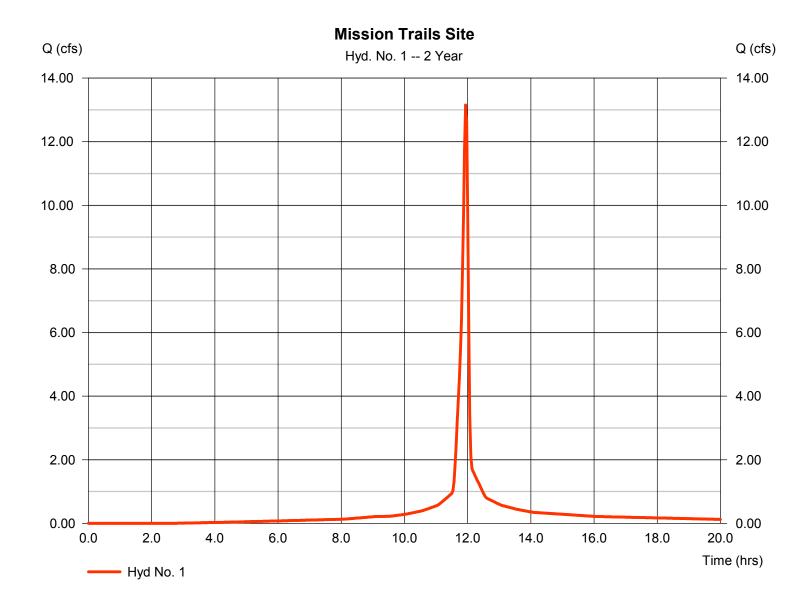
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Monday, 04 / 10 / 2017

## Hyd. No. 1

Mission Trails Site

Hydrograph type = SCS Runoff Peak discharge = 13.15 cfsStorm frequency = 2 yrsTime to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 29,148 cuft Drainage area = 2.820 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



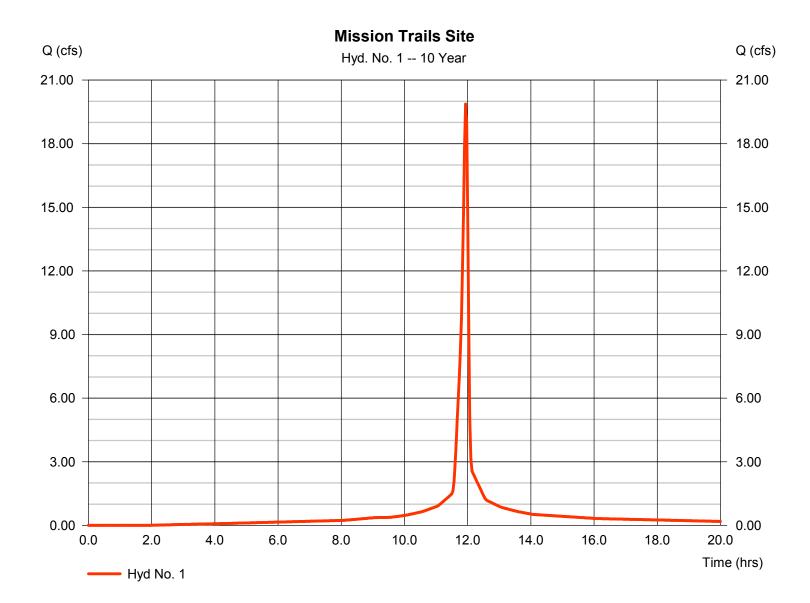
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Monday, 04 / 10 / 2017

### Hyd. No. 1

Mission Trails Site

Hydrograph type = SCS Runoff Peak discharge = 19.87 cfsStorm frequency = 10 yrsTime to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 45,267 cuft Drainage area = 2.820 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.30 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



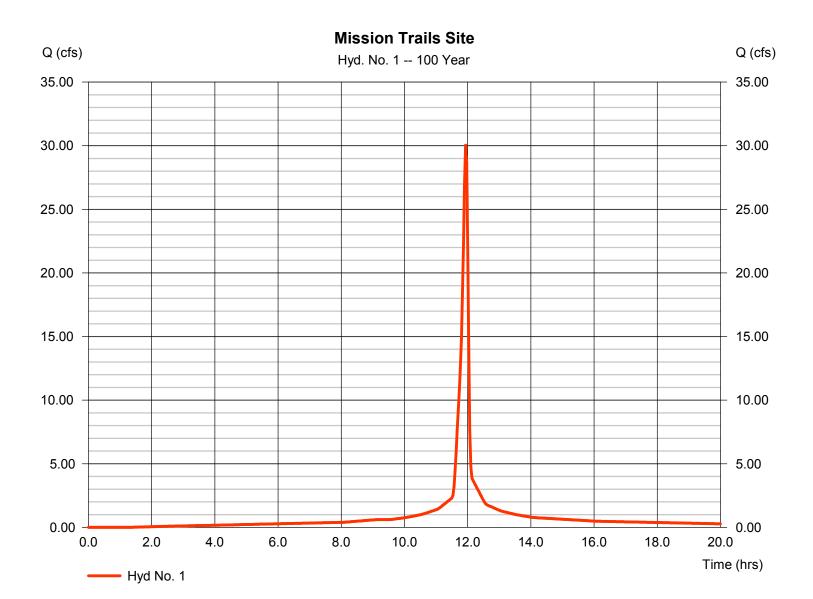
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Monday, 04 / 10 / 2017

### Hyd. No. 1

Mission Trails Site

Hydrograph type = SCS Runoff Peak discharge = 30.03 cfsStorm frequency Time to peak = 100 yrs $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 70,073 cuftDrainage area = 2.820 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.90 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



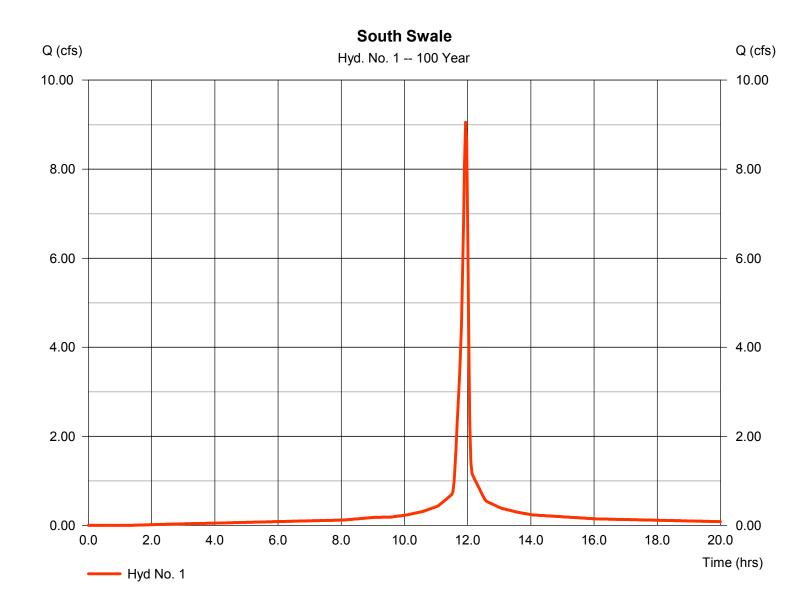
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Tuesday, 08 / 8 / 2017

### Hyd. No. 1

South Swale

Hydrograph type = SCS Runoff Peak discharge = 9.053 cfsStorm frequency = 100 yrsTime to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 21,121 cuft Drainage area Curve number = 0.850 ac= 95 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.90 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



South	Swale	Depth -	1%	Storm

	South Swale D	eptn - 1	% Storm
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
•		0.030	
Roughness Coefficient Channel Slope		2.25000	%
Left Side Slope		4.00	H:V
Right Side Slope		3.00	H:V
Bottom Width		4.00	ft
Discharge		9.05	ft³/s
			16,6
Results			
Normal Depth		0.45	ft
Flow Area		2.49	ft²
Wetted Perimeter		7.26	ft
Hydraulic Radius		0.34	ft
Top Width		7.13	ft
Critical Depth		0.47	ft
Critical Slope		0.01883	ft/ft
Velocity		3.64	ft/s
Velocity Head		0.21	ft
Specific Energy		0.65	ft
Froude Number		1.09	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.45	ft
Critical Depth		0.47	ft
Channel Slope		2.25000	%

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## South Swale Depth - 1% Storm

### **GVF Output Data**

Critical Slope 0.01883 ft/ft

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1.00 ft

1.10 ft

2.25000 %

Normal Depth Critical Depth

Channel Slope

## **South Swale - Full Flow Capcity**

### **GVF Output Data**

Critical Slope 0.01502 ft/ft

# **Existing 5'x5' RCB Capacity**

Pro	iect	Desc	rin	tion
	~~			

Friction Method Manning Formula
Solve For Discharge

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02160	ft/ft
Normal Depth	5.00	ft
Height	5.00	ft
Bottom Width	5.00	ft

#### Results

Discharge		487.29	ft³/s
Flow Area		25.00	ft²
Wetted Perimeter		20.00	ft
Hydraulic Radius		1.25	ft
Top Width		5.00	ft
Critical Depth		6.66	ft
Percent Full		100.0	%
Critical Slope		0.00739	ft/ft
Velocity		19.49	ft/s
Velocity Head		5.90	ft
Specific Energy		10.90	ft
Froude Number		1.54	
Discharge Full		487.29	ft³/s
Slope Full		0.02160	ft/ft
Flow Type	Supercritical		

#### **GVF Input Data**

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### **GVF Output Data**

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s

## **Existing 5'x5' RCB Capacity**

### **GVF Output Data**

Upstream Velocity Infinity ft/s Normal Depth 5.00 ft Critical Depth 6.66 ft Channel Slope 0.02160 ft/ft Critical Slope 0.00739 ft/ft